

Application of a dual-channel solid state spectrometer to measure spectral surface radiation and atmospheric constituents

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Introduction

- Traditional instruments (Brewers and scanning double monochromators) disadvantages:
 - Cost

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- Susceptibility to movement
- Speed of operation → limited sampling
- Solid state array instruments can overcome these, but have own drawbacks:
 - Stray light
 - Limited dynamic range
 - Temperature dependence



Aim to account for these issues in an atmospheric monitoring scenario measuring <u>direct and global spectral irradiance</u>, plus <u>ozone</u>

Overview

- Instrument description
- Calibration procedure
- Some practical considerations
- DOAS procedure and preliminary results
- Conclusions



Instrument description (1)

- Two channel diode array instrument, 512 px, 280 to 700nm, 15-bit
- Common electronics and communications
- Channel A: cosine response, Schreder optics via 5m fibre optic
- Channel B: weatherproofed direct optics, ground quartz disc attenuator





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Instrument description (2)

- Spectroradiometer also requires weatherproofing and temp stabilisation
- Weatherproofing via AI container and IP66 rated connectors
- Temperature control of entire system by PID controlled air-to-air TEM/Peltier system: $u(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau + K_d \frac{d}{dt} e(t)$
- PID constants refined at set-point of 25°C



— Ziegler and Nichols, *Trans ASME* (1942)



Calibration | Overview

- 1. Dark subtraction from raw counts
- 2. Scale to counts/s
- 3. Apply wavelength calibration
- 4. Remove stray light
- 5. Apply absolute calibration (responsivity) \rightarrow Wm⁻²nm⁻¹

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Calibration | Wavelength

• Centroid estimate: $p_{pk} = \frac{\sum p_i I_i}{\sum I_i}$

- Shortis, Clarke and Short, SPIE 2350 (1994)

- Measure two emission pencil lamps <u>simultaneously</u>: Hg and Ne
- Additionally use doublets / triplets that fall within FWHM: $\overline{\lambda} = \frac{\sum \lambda_j I_j}{\sum I_j}$



- NIST Atomic Spectra Database (2012)
- Results in 8 (13) useable emission lines
- Third order polynomial fit with r.m.s. difference of 0.18 nm (0.08 nm)
- Additional improvements via shicRIVM algorithm

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Calibration | Stray light correction (1)

• Characterised by the SDF matrix, **D**, where:

$$\mathbf{Y}_{meas} = [\mathbf{I} + \mathbf{D}]\mathbf{Y}_{IB}$$

- Can be experimentally determined from LSF measured with tuneable laser across wavelength range
- For solar UV applications, can be simplified by measuring 405 nm laser and fitting power law
 - Kreuter and Blumthaler, Rev. Sci. Instr. (2009)
- But does not achieve good fit to our data



- Zong et al, Appl. Opt. (2006)

Calibration | Stray light correction (2)

 Ideally want model-based parameterisation for stray light in diffraction grating monochromator:

 $LSF(\lambda, \lambda_M)$

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$$= \frac{\lambda_W}{\operatorname{sinc}^2 \left[\pi \left(1 - \frac{\lambda_B}{\lambda_M} \right) \right]} \left\{ \left(4 - \frac{\lambda^2}{d^2} \right)^2 \left(\frac{a^2 \sigma_r^2 q \pi^3}{d f \lambda_M^4} + \frac{\pi^2 \sigma_d^2}{\lambda_M^3} \operatorname{sinc}^2 \left[\pi \left(\frac{\lambda - \lambda_B}{\lambda_M} \right) \right] \right) + \frac{1}{\lambda_M N} \cdot \frac{1 + Nb(2\pi\lambda/\lambda_M)^2}{1 - \cos(2\pi\lambda/\lambda_M)} \cdot \operatorname{sinc}^2 \left[\pi \left(\frac{\lambda - \lambda_B}{\lambda_M} \right) \right] \right\}$$

- Sharpe and Irish, Optica Acta (1978)

$$LSF(\lambda, \lambda_M) \approx \alpha_1 \left(\frac{\lambda}{\lambda_M}\right)^4 + \alpha_2 \left(\frac{\lambda}{\lambda_M}\right)^2 + \alpha_3 + \alpha_4 \left(\frac{\lambda}{\lambda_M}\right)^{-2} + \alpha_5 \left(\frac{\lambda}{\lambda_M}\right)^{-4}$$



Calibration | Stray light correction (3)



r.m.s. difference = 5.86 x 10⁻⁶; c.f. r.m.s. for power law fit of 1.1 x 10⁻⁴

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Practical considerations

- Choice of integration time during unattended monitoring
 - Would normally take two-stage approach, but more complex in monitoring dual channel system, especially so when different optics have v. different throughputs
 - Due to single data acquisition request to instrument have to choose IT such that neither channel is saturated
 - For changeable conditions and unattended operation, select IT so that never saturated (ETSS):

$$t_{A,B} = \min\left(\frac{C_{\max}c_{A,B}(\lambda)}{I_0(\lambda)}\right)$$

- <u>Benefit</u>: can measure quasi-continuously, so little information lost, and averaging on 1 min basis reduces SNR.
- Methodology results in: <u>NEI of 0.1 mWm⁻²nm⁻¹</u>, data capture of ~16%, c.f. scanning instruments of 0.2%

DOAS retrieval

Beer's law:

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$$I(\lambda) = I_0(\lambda) \exp\left(-\alpha(\lambda)X\mu - \beta(\lambda)\frac{p_s}{p_0}m_R - \delta(\lambda)m_a\right)$$

- I_0 from ATLAS dataset, convolved with instr. slit fn.
- $\alpha(\lambda)$, O₃ cross-section, Molina and Molina (1996)
- assume λ^{-4} for Rayleigh scattering
- assume Angstrom relation for aerosol with exponent of 1.3
- multilinear regression to extract total ozone column







- SW total irradiance from CM5 pyranometer
- Study period: 31 May – 04 June 2013





r.m.s. diff = 0.83%
for μ < 3

UV WORKSHOP | PMOD/WRC, Davos, Switzerland | 28 August 2013





r.m.s. diff = 1.41%
for μ < 3

r.m.s. diff = 6.00%
for µ < 3 when
lower wavelength
limit = 306.5nm





r.m.s. diff = 1.94%
for μ < 3

• r.m.s. diff = 7.3% for μ < 3 when lower wavelength limit = 306.5nm

Summary

- Initial results promising:
 - Two channel diode array spectrometer acquiring simultaneous direct and global spectra every 1 min; now running for several months
 - Retrieved ozone values agree with calibrated Brewer to ~1% for airmasses < 3
 - Fitting LSF with model-based function improves SLC
 - Need to pay close attention to stray light correction and associated issues to extend range of airmass validity

Future work:

- Improve regression procedure; extract AOD, other species
- Analyse / compare new data over longer timescales
- Improve data filtering for partially cloudy conditions
- Inv. effect of different ozone cross-sections (Bass and Paur, Serdyuchenko etc)



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